Deriving Rewards for Reinforcement Learning from Symbolic Behaviour Descriptions of Bipedal Walking

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Abstract—Generating physical movement behaviours from their symbolic description is a long-standing challenge in artificial intelligence (AI) and robotics, requiring insights into numerical optimization methods as well as into formalizations from symbolic AI and reasoning. In this paper, a novel approach to finding a reward function from a symbolic description is proposed. The intended system behaviour is modelled as a hybrid automaton, which reduces the system state space to allow more efficient reinforcement learning. The approach is applied to bipedal walking, by modelling the walking robot as a hybrid automaton over state space orthants, and used with the compass walker to derive a reward that incentivizes following the hybrid automaton cycle. As a result, training times of reinforcement learning controllers are reduced while final walking speed is increased. The approach can serve as a blueprint how to generate reward functions from symbolic AI and reasoning.

I. Introduction

Many problems, in particular in robotics, can be phrased as optimization problems. Popular approaches to solve optimization problems are unsupervised learning techniques, such as reinforcement learning (RL) [1], [2]. RL requires both the definition of a reward function, which characterizes the quality of a solution, and an optimization algorithm to reach the maximum reward. When solving a specific problem arguably most of the time is spent on the former: the definition of a reward function that captures the essence of the desired solution, is actually maximized by the desired solution, and allows the algorithm to follow a gradient towards the desired solution. Poorly designed reward functions can lead to the algorithm getting stuck in local minima, very slow initial learning if gradients of the reward are shallow, or solutions that yield high rewards, but that do not resemble the intended target behaviour. While reward functions that yield good results for specific behaviours are discovered over time, there is no principled way of translating a symbolic description as a human would give it to a numerical reward function that leads to this behaviour if maximized. The contribution of this paper is a principled way to derive such reward functions from symbolic descriptions. We tackle the problem of bipedal walking behaviour, but the general approach can be applied to many other problems.

Walking is a highly relevant locomotion mode in robotics. Whereas there are many proven combinations of reward for-

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mulations and RL algorithms in the literature for bipedal [3], [4], [5], [6], [7] and quadrupedal [8], [4], [9], [10] robots, both in simulation and directly on real world robots [8], [11], the reward terms are mostly heuristically generated, and there is no consensus about which reward terms are necessary or sufficient. Finding a principled way to infer a reward function with minimal heuristics is the topic of inverse reinforcement learning (IRL). More precisely, IRL tries to solve the problem of inferring the reward function of an agent, given its policy or observed behaviour (see [12] for a survey). This may be complicated, as it requires a very precise understanding of the solution space; the reward function not only has to characterize the optimal solutions, it also has to guide the heuristic towards it without creating too many local minima on the way, as mentioned before. This precise understanding can be difficult to infer from observations of desired behaviour.

In contrast, humans are able to learn new behaviours from informal verbal or symbolic descriptions, also without observing demonstrations or teachers as used in IRL. Such approaches have not yet been well-studied for generating physical movements in underactuated robots. Thus, in this paper, we try to use symbolic descriptions of behaviour, as a teacher or coach could give, to derive a specific reward term for walking. For this, we use descriptions of the human gait as a succession of certain phases, such as "stance foot is in front of swing foot" or "swing leg is moving forward". At first glance, it is not straightforward to put these notions into formulas. However, these formal descriptions specify the humanoid's configuration in certain orthants of its phase space. This observation leads us to a formal characterization of the human gait given by a succession of phase space orthants. In the context of RL, we show that this characteristic can be exploited to effectively reduce the size of the search space when incorporated in the reward function. Using the compass gait as an example, we show that our method indeed improves learning times and walking speed. The simplicity of our technique should make it applicable to other walking robots or similar situations where a good reward function is hard to come by.

Organization: Section II presents the formalization of the compass walker gait as a hybrid automaton over state space orthants. Section III uses this symbolic formalization to derive a reward function term. Experimental results are presented in Section IV. Section V draws the conclusion and discusses future research directions.

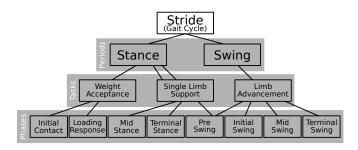


Fig. 1. Gait cycle taxonomy according to [13].

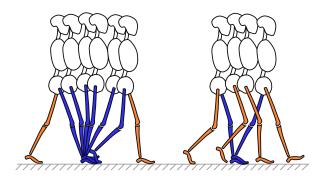


Fig. 2. An example of different phases of the human gait cycle, adapted from [13]: the stance leg (blue) supports the upper body (left), while the swing leg (orange) moves freely (right).

II. SYMBOLIC FORMALIZATION

A. From Informal to Formal Descriptions

Human walking behaviour is not easy to formalize mathematically. It consists of various phases serving a different purpose each, which are combined to an overall walking behaviour. It becomes even more complicated when considering legged locomotion variations such as running or hopping. For example, Perry [13] decomposes the stride (gait cycle) into different phases, grouped by tasks according to their function (Figure 1); different tasks accomplish weight acceptance, limb support and limb advancement (i.e. the weight is supported by one limb while the other swings forward; see Figure 2). The individual phases are described informally: "The swing foot lifts until the body weight is aligned over the forefoot of the stance leg", or "The second phase begins as the swinging limb is opposite of the stance limb. The phase ends when the swinging limb is forward and the tibia is vertical, i.e. hip and knee flexion postures are equal" ([13] pp. 9–16).

The aspect to emphasize here is that phases and especially transitions between two phases are characterized by relations of body parts, some specific joint angle, or sign changes of angular velocities. Thus, carefully defining the angles that describe a bipedal system allows us to associate each phase with a hypercube within the system's phase space. Therefore, we can give a formal characteristic of a human gait sequence by a set of hypercubes in state space and a rule in which order to traverse them. The nature of the description lends itself to a formalization in terms of hybrid automata.

In the following we apply these concepts to the compass

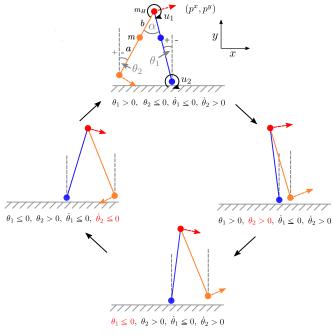


Fig. 3. Actuated compass walker cycling through the four orthants sufficient for stable walking. The stance leg is blue, the swing leg is orange. After this cycle, stance and swing leg (and hence θ_1 , θ_1 and θ_2 , θ_2) are swapped.

gait model, as a simple and well studied system to test our approach. Despite its simplicity, it can exhibit a passive walking behaviour on a slope actuated by gravity [14], [15]. We consider an actuated version on flat ground, where a virtual gravity controller can be used to generate the same gait pattern [16], [17]. We first recall the system dynamics.

B. Dynamics of the Compass Walker

The compass walker [14], [15] is a simple bipedal walker. Its two legs are called the *stance leg*, which connects with the ground and supports the weight, and the *swing leg*, which moves freely from the hip joint. It behaves like a double pendulum with a pin joint at the foot of the stance leg. Consequently, its dynamics are described as follows:

$$M(\theta)\ddot{\theta} + C(\theta, \dot{\theta}) + g(\theta) = \mathbf{S}u$$
 (1)

with $\boldsymbol{\theta} = [\theta_1, \theta_2]^T$ being the configuration vector, where θ_1 is the angle of the stance leg to the upright, and θ_2 is the angle between the swing leg and the upright, $\boldsymbol{u} = [u_1, u_2]^T$ the torque vector, with u_1 the torque at the hip and u_2 the torque at the ankle, and (p^x, p^y) the coordinates of the hip joint (cf. Figure 3).

Gravity acts according to

$$g(\theta) = g \begin{bmatrix} -(m_H l + ma + ml)\sin(\theta_1) \\ mb\sin(\theta_2) \end{bmatrix}$$
(2)

where m is the mass of leg, given as single mass point at a from the foot, l=a+b is the length of the leg, and m_H is the mass point at the hip (cf. Figure 3). Control acts on the system via

$$S = \begin{bmatrix} 1 & 1 \\ 0 & -1 \end{bmatrix} \tag{3}$$

Inertial and Coriolis matrices are described by

$$M(\boldsymbol{\theta}) = \begin{bmatrix} m_H l^2 + ma^2 + ml^2 & -mbl\cos(\theta_1 - \theta_2) \\ -mbl\cos(\theta_1 - \theta_2) & mb^2 \end{bmatrix}$$
(4)
$$C(\boldsymbol{\theta}, \dot{\boldsymbol{\theta}}) = \begin{bmatrix} 0 & -mbl\sin(\theta_1 - \theta_2)\dot{\theta}_2 \\ mbl\sin(\theta_1 - \theta_2)\dot{\theta}_1 & 0 \end{bmatrix}$$
(5)

Ground collision of the swing leg occurs when it is in front of the stance leg, the task space velocity of the swing leg is negative in y, and $y=0.^1$ When ground contact occurs, swing and stance leg immediately change roles and the angular momentum is transferred assuming a perfectly inelastic collision. This means θ_1 gets assigned to θ_2 and vice versa, and the transition of angular velocities is calculated via

$$\mathbf{T}^{+}(\alpha)\dot{\boldsymbol{\theta}}^{+} = \mathbf{T}^{-}(\alpha)\dot{\boldsymbol{\theta}}^{-} \tag{6}$$

$$\dot{\boldsymbol{\theta}}^{+} = \mathbf{T}^{+}(\alpha)^{-1}\mathbf{T}^{-}(\alpha)\dot{\boldsymbol{\theta}}^{-} \tag{7}$$

where $^+/^-$ denote states right after/before collision and $\alpha=\theta_1^--\theta_2^-=\theta_2^+-\theta_1^+$ is the inter-leg angle at the moment of transition. The transition matrices are given by

$$\mathbf{T}^{+}(\alpha) = \begin{bmatrix} m_{H}l^{2} + ma^{2} + ml(l - bc_{\alpha}) & mb(b - lc_{\alpha}) \\ -mblc_{\alpha} & mb^{2} \end{bmatrix}$$
$$\mathbf{T}^{-}(\alpha) = \begin{bmatrix} (m_{H}l^{2} + 2mal)c_{\alpha} - mab & -mab \\ -mab & 0 \end{bmatrix}$$

where $c_{\alpha} = \cos(\alpha)$. This formulation largely follows [16], [17], further mathematical details can be found in [14].

C. A Formal Model of Ideal Walking

Now, the link has to be made to relate the states of these dynamics with the walking phase descriptions mentioned above. The crucial observation is that the different phases are determined by whether the swing leg is to the left or to the right of the stance leg, whether the stance leg is leaning left or right and whether the legs are moving clockwise or counter-clockwise around their respective joints. This can be described in terms of θ_1 , θ_2 and the corresponding angular velocities $\dot{\theta}_1$ and $\dot{\theta}_2$, which spans the phase space x= $[\theta_1, \theta_2, \dot{\theta}_1, \dot{\theta}_2]^T$ of the compass walker. Figure 3 shows this decomposition, where the swing leg starts from its hindmost position and swings all the way to the front, when it becomes the stance leg. The case distinction of $\theta_1, \theta_2, \theta_1, \theta_2$ being smaller or larger than zero yields sixteen partitions (orthants) of the state space, and the observation above defines a cycle involving only four of these. In the following section, we give a formal model of this ideal walking behaviour. We then use this model to construct a reward function which encourages the compass walker to adhere to this formal model; in other words, we reward walking "properly".

The formal model of ideal walking behaviour consists of a cycle of the four orthants sufficient for stable walking. It is based on hybrid automata, as introduced by Alur

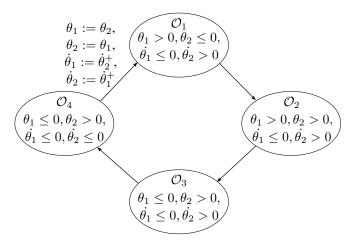


Fig. 4. Hybrid automaton modelling the orthant sequences. $\dot{\theta}^+ = [\dot{\theta}_1^+, \dot{\theta}_2^+]^T$ is calculated according to the impulse transition equation (7).

[18] and Henzinger [19]. Hybrid automata allow combining continuous behaviour with discrete states. Briefly, a hybrid automaton is given as a tuple

$$\mathcal{H} = (V_D, Q, E, \mu_1, \mu_2, \mu_3) \tag{8}$$

where V_D is a set of n real-valued data variables valued in $\Sigma_D = \mathbb{R}^n$, Q is a set of locations (discrete states), and E is a transition relation $E \subseteq Q \times Q$ between the states. Further, for each $q \in Q, \sigma \in \Sigma_D, \mu_1(q)$ is a set of activities specified by differential equations, $\mu_2(q,\sigma)$ is an invariant predicate, and for each $e \in E, \sigma, \tau \in \Sigma_D, \mu_3(e,\sigma,\tau)$ is a transition relation between data variables. Intuitively, the automaton starts in a state $q \in Q$ with data variables set to $\sigma \in \Sigma_D$ s.t. $\mu_2(q,\sigma)$ is true. The continuous behaviour of the data variables is specified by $\mu_1(q)$. As soon as the predicate $\mu_2(q,\sigma)$ becomes false, the automaton transitions into a state $p \in Q$ where $(q,p) \in E$; the values of the data variables may then change into $\tau \in \Sigma_D$ such that $\mu_3((p,q),\sigma,\tau)$ is true.

Here, the state variables are given by $\theta_1, \theta_2, \dot{\theta}_1, \dot{\theta}_2$, and we have four locations, corresponding to the states in Figure 3:

$$V_D = \{\theta_1, \theta_2, \dot{\theta}_1, \dot{\theta}_2\} \tag{9}$$

$$Q = \{ \mathcal{O}_1, \mathcal{O}_2, \mathcal{O}_3, \mathcal{O}_4 \} \tag{10}$$

The activities $\mu_1(q)$ for $q \in Q$ are given by the differential equations (1) to (5). The invariants specify the orthants in the system state as follows:

$$\mu_2(\mathcal{O}_1) \Longleftrightarrow \theta_1 > 0 \land \theta_2 \le 0 \land \dot{\theta_1} \le 0 \land \dot{\theta_2} > 0$$
 (11)

$$\mu_2(\mathcal{O}_2) \iff \theta_1 > 0 \land \theta_2 > 0 \land \dot{\theta_1} \le 0 \land \dot{\theta_2} > 0$$
 (12)

$$\mu_2(\mathcal{O}_3) \Longleftrightarrow \theta_1 \le 0 \land \theta_2 > 0 \land \dot{\theta_1} \le 0 \land \dot{\theta_2} > 0$$
 (13)

$$\mu_2(\mathcal{O}_4) \Longleftrightarrow \theta_1 \le 0 \land \theta_2 > 0 \land \dot{\theta_1} \le 0 \land \dot{\theta_2} \le 0$$
 (14)

The transition relation E specifies the cycle mentioned above, and corresponds to the arrows between the four states in Figure 3:

$$E = \{ (\mathcal{O}_1, \mathcal{O}_2), (\mathcal{O}_2, \mathcal{O}_3), (\mathcal{O}_3, \mathcal{O}_4), (\mathcal{O}_4, \mathcal{O}_1) \}$$
 (15)

¹Notice that during the forward swing, the swing leg will penetrate or touch the ground due to the simplified model assumptions (*i.e.* no knee joint is included); we disregard this in our simulation.

²Note that although our model is deterministic, in general hybrid automata can be non-deterministic.

When a transition occurs, μ_3 specifies the possible values of $\theta_1, \theta_2, \dot{\theta}_1, \dot{\theta}_2$. This mapping is the identity, except at the last transition $(\mathcal{O}_4, \mathcal{O}_1)$, where θ_1 and θ_2 are interchanged, and the impulse is transferred between $\dot{\theta}_1$ and $\dot{\theta}_2$:

$$\mu_{3}(p,q) = \begin{cases} \{(\theta_{1},\theta_{2}), (\theta_{2},\theta_{1}), (\dot{\theta}_{1},\dot{\theta}_{2}^{+}), (\dot{\theta}_{2},\dot{\theta}_{1}^{+})\} \\ \text{if } p = \mathcal{O}_{4}, q = \mathcal{O}_{1} \\ \{(\theta_{1},\theta_{1}), (\theta_{2},\theta_{2}), (\dot{\theta}_{1},\dot{\theta}_{1}), (\dot{\theta}_{2},\dot{\theta}_{2})\} \\ \text{otherwise} \end{cases}$$
(16)

where $\dot{\theta}^+ = [\dot{\theta}_1^+, \dot{\theta}_2^+]^T$ is calculated according to the impulse transition equation (7). The automaton defined by equations (9) to (16) can also be described by a diagram (*cf.* Figure 4). The diagram shows the states, the state invariants defined by μ_2 , the state transitions in E, and the change of the state variables after the transitions defined by μ_3 ; it does not show the identities in (16), *i.e.* $\theta_1 := \theta_1, \theta_2 := \theta_2$, *etc.* in all other transitions, as this is usually elided, and for clarity we also do not show the activities (defined by μ_1) in the diagram.

III. REWARD FORMULATION

For an agent to make use of this exploration space reduction given by the hybrid automaton formulation, we define the orthant reward term $r_{\rm or}$ as:

$$r_{\text{or}}(\boldsymbol{x}_{t}, \boldsymbol{x}_{t-1}) = \begin{cases} +1 & \text{if} & \mathcal{O}(\boldsymbol{x}_{t-1}) \in Q \land \\ & \mathcal{O}(\boldsymbol{x}_{t}) \in Q \land \\ & (\mathcal{O}(\boldsymbol{x}_{t-1}), \mathcal{O}(\boldsymbol{x}_{t})) \in E \\ +1 & \text{if} & \mathcal{O}(\boldsymbol{x}_{t-1}) \notin Q \land \\ & \mathcal{O}(\boldsymbol{x}_{t}) \in Q \\ -1 & \text{else} \end{cases}$$

$$(17)$$

Here, Q, E refer to the definitions of the hybrid automaton of ideal walking from Section II-C, and $\mathcal{O}(x)$ maps the state x to the current orthant \mathcal{O}_k , $k \in \{1, ..., 16\}$. This reward is visualized in Figure 5; essentially, it incentivizes the walker to follow the sequence of the formal model developed in Section II-C.

As comparison, we also consider a reward which is commonly used in locomotion tasks, namely rewarding task space motion in the intended direction. This reward reads

$$r_{\text{for}}(\boldsymbol{p}_t, \boldsymbol{p}_{t-1}) = 2H(p_t^x - p_{t-1}^x) - 1$$
 (18)

where H denotes the Heaviside function, and $p_t = (p_t^x, p_t^y)$ the task space coordinates of the hip joint (see Figure 3). Further, rewards are used to encourage smooth controls (r_{jerk}) , high walking distance (r_{dist}) , and punish falling (r_{fall}) . These terms are defined as:

$$r_{\text{jerk}}(\boldsymbol{u}_t, \boldsymbol{u}_{t-1}) = ||\boldsymbol{u}_t - \boldsymbol{u}_{t-1}||_2$$
 (19)

$$r_{\text{dist}}(\boldsymbol{p}_t, t) = p_t^x H(t - T)x \tag{20}$$

$$r_{\text{fall}}(\boldsymbol{p}_t) = H(-p_t^y) \tag{21}$$

The full reward is then given as

$$r(\boldsymbol{x}_{t}, \boldsymbol{x}_{t-1}, \boldsymbol{p}_{t}, \boldsymbol{p}_{t-1}, \boldsymbol{u}_{t}, \boldsymbol{u}_{t-1}, t) =$$

$$\omega_{\text{jerk}} r_{\text{jerk}}(\boldsymbol{u}_{t}, \boldsymbol{u}_{t-1}) + \omega_{\text{dist}} r_{\text{dist}}(\boldsymbol{p}_{t}, t) +$$

$$\omega_{\text{fall}} r_{\text{fall}}(\boldsymbol{p}_{t}) + \omega_{\text{for}} r_{\text{for}}(\boldsymbol{p}_{t}, \boldsymbol{p}_{t-1}) + \omega_{\text{or}} r_{\text{or}}(\boldsymbol{x}_{t}, \boldsymbol{x}_{t-1})$$
(22)

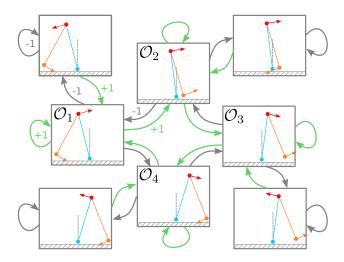


Fig. 5. Visualization of the orthant reward term defined in equations (17). Staying in the stable orthant cycle or entering the cycle is rewarded with +1, exiting the cycle or moving in the wrong direction is punished with -1. Not all possible orthants are shown for clarity.

IV. RESULTS AND DISCUSSION

Using the previously mentioned formulation, we compared training setups of reward configurations in terms of reward optimization and highest achieved walking distance.³ The observation in the RL setup was the robot configuration x_t . Thus, a policy $\pi(x_t) \to u_t$ was trained mapping the configuration state to the control input. As training algorithm, PPO was chosen [20] in the stable-baselines3 implementation [21] with default parameters. We evaluate different combinations of reward terms to disentangle the effects of the various terms. The different reward setups are detailed in Table I. The other weights in equation (22) were set to

TABLE I
WEIGHTS FOR THE REWARD TERMS

	sparse	for	or	for + or
$\omega_{ m for}$	0.0	0.01	0.0	0.005
$\omega_{ m or}$	0.0	0.0	0.01	0.005

 $\omega_{\rm jerk}=-0.001, \omega_{\rm dist}=1, \omega_{\rm fall}=-10.$ A training episode was terminated if a fall occurred, *i.e.* if $r_{\rm fall}(\boldsymbol{p}_t)=1$, or the maximal episode length of T=10 s was reached. Each training condition was run 15 times with different random seeds and 500000 environment steps per run.

As a baseline comparison, we use the virtual gravity controller

$$\mathbf{S}\boldsymbol{u}_{vg} = \begin{bmatrix} (m_H l + m(a+l))\cos(\theta_1) \\ -mb\cos(\theta_2) \end{bmatrix} g\tan(\phi) \qquad (23)$$

described in [17], simulating passive walking on a slope of $\phi = -0.07$ rad. The parameters of the compass walker plant used in all simulations is given in Table II, and the initial condition for all experiments was $\mathbf{x}_0 = [0.0, 0.0, -0.4, 2.0]^T$.

³Accompanying code is publicly available at https://github.com/dfki-ric-underactuated-lab/orthant_rewards_biped_rl

TABLE II
PHYSICAL PARAMETERS OF THE COMPASS GAIT WALKER

m_H	m	a	b	l
1 kg	0.5 kg	0.5 m	0.5 m	1.0 m

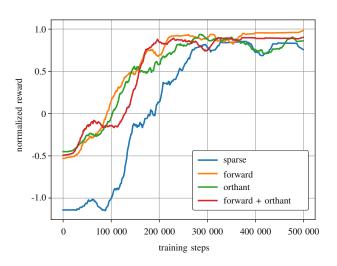


Fig. 6. Averaged learning curves for different rewards. The virtual gravity controller from equation (23) serves as baseline to which the rewards are normalized

Figure 6 shows the averaged learning curves for the different reward setups, normalized to the reward gained by the virtual gravity baseline controller. Whereas reward setups using forward or orthant reward terms reach close to optimal reward values earlier in training, after around 200000 steps, convergence is slower for the sparse setup. Figure 7 compares the highest achieved walking distance for each reward setup, taken over the 15 runs per setup.⁴ Here, the combined reward of orthant reward and forward velocity reward leads to the fastest convergence and highest achieved walking distance. Similar walking distances are reached after considerably longer time in both individual reward setups of only orthant reward and only forward velocity reward. Strikingly, walking distances for the sparse setup also converge, but at markedly lower values. The standard deviation of the highest achieved reward highest achieved walking distance are shown in Table III.

In summary, whereas a sparse reward setup reaches comparable performance to the baseline virtual gravity controller, both the typically used forward velocity reward and the novel orthant reward improve the performance, with the combination of both reaching the highest performance. The orthant reward leads to the lowest standard deviation of the performance across trials, making it the most reproducible method in our study. The combination of the orthant and forward reward has an increased standard deviation, however below the values for the sparse reward. Interestingly, both forward and orthant rewards seem redundant: Observing a stable compass gait, both the predicates of 'forward hip velocity is positive' and 'orthant sequence follows the stable

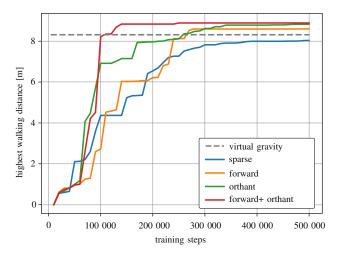


Fig. 7. Highest walking distances achieved for t=10s for different rewards. The virtual gravity controller from equation (23) serves as baseline. All reward setups result in higher walking distances than the reference, except for the sparse setup. A combination of forward and orthant reward terms yields the highest improvements.

TABLE III STANDARD DEVIATIONS

setup	sparse	forward	orthant	fwd+ orthant
reward	0.127	0.045	0.039	0.088
walking distance	1.302	1.192	0.744	1.173

orthant gait cycle' are always true. Yet the combination of both incentives through the reward function is more successful in reaching higher walking distances than each incentive on its own, at the cost of a slightly reduced reproducibility indicated by the increased standard deviation. This is part of a long-standing question in reward shaping, where the optimal combination of reward terms to achieve a goal is unclear. Too many redundant terms can deteriorate learning, whereas too little guidance can lead to impractical training times or no convergence at all. In comparison to typically used reward terms, the orthant reward is simple and straight forward since it amounts to a single truth value telling the agent whether it is close to the set of desired phase space trajectories.

V. CONCLUSION AND OUTLOOK

This paper has presented a first attempt towards creating a link between symbolic reward formulation based on informal descriptions of behaviour and behaviour policy generation. The main novelty of our approach is a systematic way to derive a reward function from an informal description of the desired behaviour in three steps employing well-understood mathematical techniques: (i) from an informal description of the behaviour, we have derived a formal specification of the desired behaviour as a hybrid automaton; (ii) the hybrid automaton is an abstraction of the state space of the system, *i.e.* a restriction of its phase space; (iii) this restriction allowed to formulate a better reward function for reinforcement learning. We have demonstrated that this kind of input is useful in speeding up the learning process of

⁴See accompanying video at https://youtu.be/CkvLvz_tLtc.

achieving stable bipedal locomotion; the key here is the effective search space reduction given by the formal model.

It is worth pointing out that although we derive an effective reward function, the main contribution of this paper is the way in which the combination of symbolic description and reinforcement learning improves the overall result; this should work with other reinforcement learning techniques and reward functions as well, but to what degree remains to be investigated. It further remains an open problem to figure out what is the right granularity to seek in reward shaping. For example, it is interesting to study if splitting the orthants into smaller hypercubes and coming up with more fine-grained rules will bring additional improvements in the learning process. Furthermore, this formalization naturally lends itself to applications in curriculum learning, where a coarse grained initial formulation can be made more detailed when the agent reaches a certain proficiency, which could potentially even more effectively guide the learning agent.

This kind of symbolic reward definition maybe be combined with existing inverse reinforcement learning techniques to automatically derive reward specifications for any given behaviour. For example, there is no principal reason why this technique should not work for walking robots with higher degrees of freedom, except that for these the formal model as a hybrid automaton may be not as straightforward to formulate as for the compass walker. In future work, we want to investigate how the present method can be applied to more complex humanoid walking robots (such as [22]) using the basics developed here combined with mapping template models to whole body control.

Another aspect worth exploring is proving properties (such as safety properties) about the controlled system. Here, the formalization as a hybrid automaton has the advantage that powerful tool support exists [23], [24]. This can be used to show that learned behaviours satisfy given properties [25], so our approach can also be used for safety verification of learned robot behaviours. This would be an enormous advantage over existing approaches, where a safety guarantee for learned behaviours cannot be given.

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